

**THE NATIONAL UNIVERSITY OF IRELAND, GALWAY**

International Postgraduate Hydrology Course

**Higher Diploma (Hydrology) - Summer Examinations, 2000**

**APPLIED HYDROLOGY I (EH 864)**

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**Time allowed is *three hours*.      Attempt *any five* questions**

*(The Handout provided may be useful in one or more questions).*

1. (a) In the context of a continuous linear time-invariant system, initially relaxed, demonstrate *graphically* the operation of the "convolution" of two time functions.
- (b) Does the operation of convolution imply that the system is necessarily conservative? *(Briefly explain your answer!)*
- (c) Is the application of the convolution integral generally a practical option in the hydrological context? *(Explain your answer in one sentence!)*
- (d) For a system defined by the convolution integral, derive relations between:
  - (i) the unit step response function  $S(t)$  and the unit impulse response function  $h(o,t)$ .
  - (ii) the unit pulse (of duration  $T$ ) response function  $h(T,t)$  and the unit impulse response function  $h(o,t)$ .
  - (iii) the unit pulse response function  $h(T,t)$  and the unit step response function  $S(t)$ .
- (e) Demonstrate that the convolution summation relation

$$y_m = \sum_{r=0}^m x_r h_{m-r} \quad \text{for } m = 0, 1, 2, 3, \dots,$$

is discretely coincident with the assumed convolution integral relation

$$y(t) = \int_0^t x(\tau) \cdot h(0, t - \tau) \cdot d\tau$$

between the *volumes* of the effective rainfall blocks and the *ordinates* of the storm-runoff component of the total discharge hydrograph.

- (f) State clearly any other conditions which yield the convolution summation relation as a discretely coincident form of the continuous linear model.

2. (a) What (*very briefly!*) do you understand by each of the following terms:

flood routing,                  reservoir routing,                  channel routing,  
linear routing,                  forward-routing          and          back-routing.

(b) In the context of **channel routing** for an isolated storm event, show that the outflow discharge peak value  $Q_p = Q(t_p)$  is *higher* and occurs *later* than the discharge value associated with the time  $t_m$  when the inflow *just equals* the outflow.

(c) Demonstrate that the Muskingum channel routing model, defined by the storage( $S$ )-inflow( $I$ )-outflow( $Q$ ) relation  $S(t) = K [X.I(t) + (1 - X).Q(t)]$ , where  $K$  and  $X$  are constant parameters, is a *linear* one?

(d) Outline the derivation of the expressions for the coefficients  $C_0$ ,  $C_1$ , and  $C_2$  of the classic finite-difference form of the Muskingum channel routing model, having the general form

$$Q_m = C_0 Q_{m-1} + C_1 I_m + C_2 I_{m-1}, \quad \text{for } m = 0, 1, 2, \dots$$

and discuss *briefly* the restrictions (if any) on the model parameters  $K$  and  $X$  and on the data interval  $T$ .

(e) Show that, for the routing system to be conservative, the coefficients of any discrete form of the Muskingum model must satisfy the relation

$$(C_0 + C_1 + C_2) = 1$$

(f) Indicate *briefly* the physically unrealistic characteristic of the unit impulse response function of the Muskingum model and its implication in the application of the method.

3. (a) Using the continuity equation, or otherwise, show *algebraically* that, in the case of **reservoir routing**, for an isolated storm event, the peak of the outflow hydrograph always lies at a point on the recession curve of the inflow hydrograph, this point corresponding to time  $t_m$ .

(b) Briefly explain the Modified Puls Method for routing a *given* inflow hydrograph through a non-linear reservoir, given also the *initial* outflow and the storage-discharge relation for the outflow control.

(c) An artificial lake, of area  $1 \text{ km}^2$ , with vertical sides, is controlled by a broad-crested weir having the discharge/upstream-head relation  $Q = 1.705 B H^{3/2} \text{ m}^3\text{s}^{-1}$ , the width of the weir being  $B = 5 \text{ m}$ . Given that the initial water surface level in the lake is *just at* the crest of the weir, check *any two consecutive outflow values* in the following computer output table, for the *given* inflow hydrograph, taking the routing period  $T = 6 \text{ hours}$ .

Time $t$ (hours)	0	6	12	18	24	30	36	42
Inflow $I$ ( $\text{m}^3\text{s}^{-1}$ )	0	15	25	45	60	40	30	0
Outflow $Q$ ( $\text{m}^3\text{s}^{-1}$ )	0	0.5269	3.4350	10.5240	22.7720	31.9730	33.0474	26.7901

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(d) If the lake area  $A$  is reduced by 10%, e.g. by a landslide, what corresponding new value of the weir width  $B$  would yield *exactly* the same outflow data as that given above, for the *same* inflow hydrograph and the *same* initial storage conditions?

4. (a) In the context of unit hydrograph theory, what (*very briefly*) do you understand by each of the following terms:
- (i) base flow, (ii) storm runoff, (iii) effective (excess) rainfall,
  - (iv) the instantaneous unit hydrograph (the IUH), (v) the unit S-curve, and
  - (vi) the unit hydrograph of duration  $T$  (the TUH).

(b) Suppose that the direct *storm runoff*, sampled at intervals of  $T = 2$  hours, up to time  $t = 34$  hours, due to 1 cm of *effective* rainfall falling *uniformly* on a catchment over a period of time  $2T = 4$  hours, is as tabulated below.

Time $t$ (hours)	0	2	4	6	8	10	12	14	16
Storm Runoff ( $\text{m}^3\text{s}^{-1}$ )	0.0	83.33	141.66	99.16	69.42	48.59	34.01	23.81	16.67
Time $t$ (hours)	18	20	22	24	26	28	30	32	34
Storm Runoff ( $\text{m}^3\text{s}^{-1}$ )	11.67	8.17	5.72	4.00	2.80	1.96	1.37	0.96	0.67

Estimate

(i) the value (in  $\text{m}^3\text{s}^{-1}$ ) of the unit S-curve at time  $t = 8$  hours

(ii) the time to peak and the magnitude of the peak of the 4-hour unit hydrograph  $h(2T, mT)$

(iii) the time to peak and the magnitude of the peak of the 6-hour unit hydrograph  $h(3T, mT)$

(iv) the time to peak and the magnitude of the peak of the 2-hour unit hydrograph  $h(T, mT)$ .

(c) If the area of the catchment considered in (b) above is  $A = 400 \text{ km}^2$ , determine the *theoretical* value of the sum of *all* of the ordinates of

(i) the 4-hour unit hydrograph

(ii) the 6-hour unit hydrograph

(iii) the 2-hour unit hydrograph

where each unit hydrograph is sampled at intervals of  $T = 2$  hours.

(d) Why is it generally more difficult to derive a satisfactory estimate of a shorter duration unit hydrograph from a longer one and vice versa?

(e) What do you perceive as the fundamental weaknesses of the unit hydrograph theory?

5. (a) Explain, *very briefly*, why the Linear Transfer (LTF) model, defined by

$$(1 + \phi_1 B + \phi_2 B^2 + \dots + \phi_n B^n) y_m = (\theta_0 + \theta_1 B + \theta_2 B^2 + \dots + \theta_k B^k) x_m, \text{ for } m = 0, 1, 2, 3, \dots,$$

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where  $B$  is the *backward shift operator* and  $n > k$ , is still widely used in deterministic hydrological modeling, particularly in the context of real-time river flow forecasting.

- (b) Show that the Gain Factor ( $G$ ) of the LTF model is given by

$$G = \frac{\theta_0 + \theta_1 + \theta_2 + \dots + \theta_k}{1 + \phi_1 + \phi_2 + \dots + \phi_n}$$

- (c) For the discrete cascade model of two unequal discrete linear reservoirs, defined by

$$(1 + K_1 \nabla)(1 + K_2 \nabla)y_m = x_m, \quad \text{for } m = 0, 1, 2, 3, \dots$$

where  $\nabla$  is the *backward difference operator*, with  $\nabla = (1 - B)$ , show that

- (i) the model is conservative,

- (ii) its unit impulse response series is given by

$$h_m = \frac{(1 - q_1)(1 - q_2)}{(q_1 - q_2)} [q_1^{m+1} - q_2^{m+1}], \quad \text{for } m = 0, 1, 2, 3, \dots,$$

$$\text{where } q_1 = \frac{K_1}{1 + K_1} \text{ and } q_2 = \frac{K_2}{1 + K_2},$$

- (iii) its lag (i.e. the 1<sup>st</sup> moment about the origin) is  $M_1' = (K_1 + K_2)$ .

- (d) If only two isolated blocks of effective rainfall, 2cm and 1cm in depth, each of duration  $T = 2$  hours, fall on a catchment of area  $A = 360 \text{ km}^2$ , determine the first five ordinates of the storm runoff, at 2-hour intervals, assuming that the form of LTF model in part (c) above is appropriate, with  $K_1 = 4$  and  $K_2 = 2$ , using *either* the linear difference equation *or* convolution summation.

6. (a) For a linear reservoir, defined by the storage-discharge relation  $S(t) = K.Q(t)$ , where  $K$  is a constant and  $t$  is time, show in outline that its discretely-coincident form (CDF), for the case of pulsed (i.e. histogram-type) inputs, is

$$(1 - qB).Q_m = (1 - q).I_m \quad \text{for } m = 0, 1, 2, 3, \dots,$$

where  $q = e^{-\frac{T}{K}}$ ,  $T$  is both the duration of the input pulses and the sampling interval,  $B$  is the backward shift operator and  $I_m$  and  $Q_m$  are the intensities of the input pulses and the sampled outflow hydrograph ordinates respectively.

- (b) Describe the main steps involved in the construction of the Clark instantaneous unit hydrograph (IUH), with particular reference to the determination of the isochrones of equal travel time, the time of concentration  $T_c$ , the time-area diagram and the storage coefficient  $K$  of the continuous linear reservoir at the outlet of the catchment.  
(A clear diagram would be helpful!)

- (c) The following table shows the **time-area diagram** (as areas between **isochrones**) for a catchment having an area  $A = 110 \text{ km}^2$  and a time of concentration  $T_c = 18$  hours. For the **Clark model**, find the **IUH** of this catchment. Assume that the storage coefficient of the linear reservoir at the outlet of watershed is  $K = 12$  hours.

Travel Time (hours)	0-2	2-4	4-6	6-8	8-10	10-12	12-14	14-16	16-18
Inter-isochrone area (km <sup>2</sup> )	3	9	20	22	16	18	10	8	4

- (d) Is the Clark IUH model still used ? *Briefly* explain your answer!

7. (a) What are the two *principal* components or modules common to most **conceptual rainfall-runoff models**? *Very briefly*, explain the role of each of these modules in the overall operation of the model.

- (b) With reference to the schematic line diagram of the Liang version of the **Soil Moisture Accounting and Routing (SMAR)** model, provided with the **Formula Handout**, explain *briefly but unambiguously* the operation of the model over a single data interval of time, (i.e. one day) when

- (i) when the rainfall depth is *less than or equal* to the potential evapotranspiration depth, assuming that *all* of the soil layers are full of moisture.

- (ii) when the rainfall depth is *greater than* the potential evapotranspiration depth assuming that *not all* of the soil layers are full of moisture.

- (c) Suppose that the **optimised parameters** of the **water balance component** of the SMAR model are given as:

$T = 0.9$ ,  $H = 0.25$ ,  $Y = 100 \text{ mm/day}$ ,  $Z = 40 \text{ mm}$  and  $C = 0.8$  and and that the **rainfall (R)** and **pan-evaporation (E)** data for three consecutive days on the chosen catchment are as follows:

Rainfall in mm/day:                      0                      15                      40

Pan Evap. in mm/day:                      30                      20                      10

Assuming that *all* of the soil layers are *initially* full of moisture, check the results in the table below for the **outputs of the water balance module**.

Time Interval	$r_1$ (mm/day)	$r_2$ (mm/day)	$r_3$ (mm/day)	$E_a$ (mm/day)	$S_{t,1}$ (mm)	$S_{t,2}$ (mm)
Day-1	0.0	0.0	0.0	26.6	0.0	13.4
Day-2	0.0	0.0	0.0	17.4	0.0	11.00
Day-3	2.13125	0.0	0.0	9.0	25.0	14.86875

### *Summary of results for the water balance module of the SMAR model*

(Please note that  $r_1$  denotes the direct generated runoff,  $r_2$  the generated runoff in excess of infiltration ( $Y$ ),  $r_3$  the generated runoff in excess of the moisture capacity ( $Z$ ) of the soil layers,  $S_{t,1}$  and  $S_{t,2}$  the final storage depths of layers one and two respectively at the end of each day and  $E_a$  the actual evaporation).